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# Excess molar enthalpies of methyl *tert*-butyl ether + (cyclohexane or 2,3-dimethylbutane) + n-decane ternary mixtures at 298.15 K

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#### Abstract

Microcalorimetric measurements of the excess molar enthalpies at 298.15 K are reported for the ternary mixtures methyl *tert*-butyl ether + (cyclohexane or 2,3-dimethylbutane) + ndecane. Smooth representations of the results are presented and used to construct constant enthalpy contours on a Roozeboom diagram. Application of the Flory theory of mixtures to estimate the enthalpies of the ternary mixtures from analyses of data for their constituent binaries is also described.

## INTRODUCTION

The use of methyl *tert*-butyl ether (MTBE) as a gasoline-blending agent has led to an increased interest in the thermodynamic properties of mixtures of MTBE with hydrocarbons. A recent paper [1] from our laboratory reported the excess molar enthalpies  $H_m^E$  of the ternary system MBTE + *n*hexane + *n*-decane at 298.15 K. As an extension of that work, similar measurements have been made for the ternary systems MTBE + cyclohexane + *n*-decane, and MTBE + 2,3-dimethylbutane (23DMB) + *n*-decane, in which different C<sub>6</sub>-hydrocarbons replace the *n*-hexane used previously.

## EXPERIMENTAL

## **Materials**

The MTBE (HPLC grade) used was obtained from the Aldrich Chemical Co. The cyclohexane and 23DMB were Pure Grade materials from the Phillips Chemical Co. All of these materials had stated purities exceeding 99 mol%. The *n*-decane was the same as used in our previous work [1, 2].

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At 298.15 K, the densities of the component liquids were 735.56, 774.04, 657.13 and 726.29 kg m<sup>-3</sup> for MTBE, cyclohexane, 23DMB and *n*-decane, respectively.

## Equipment and technique

The excess molar enthalpies were measured at 298.15 K in a flow microcalorimeter maintained within  $\pm 0.002$  K of the nominal operating temperature. The equipment and experimental procedure were the same as in our previous work [1]. In studying the ternary systems, the excess molar enthalpy  $H_{m,1+23}^{E}$  was measured for several pseudo-binary systems in which component 1 (MTBE) was added to a binary mixture of components 2 (cyclohexane or 23DMB) and 3 (*n*-decane) having a fixed mole ratio  $x_2/x_3$ . These binaries were prepared by weighing. The excess molar enthalpy  $H_{m,123}^{E}$ was then obtained from the relation

$$H_{m,123}^{E} = H_{m,1+23}^{E} + (1 - x_1)H_{m,23}^{E}$$
<sup>(1)</sup>

where  $H_{m,23}^{E}$  is the excess molar enthalpy of the particular binary mixture. Values of  $H_{m,23}^{E}$  for cyclohexane + *n*-decane and for 23DMB + *n*-decane were taken from the literature [3, 4]. The errors in  $H_{m,1+23}^{E}$  are estimated to be less than 0.5% over most of the MTBE mole fraction range. Errors in the mole fractions of the final ternary mixtures are estimated to be less than  $5 \times 10^{-4}$ .

# **RESULTS AND DISCUSSION**

The values of  $H_{m,12}^{E}$  measured for the binary mixture MTBE + cyclohexane are listed in Table 1. A Redlich-Kister form, representing the data, is given in the footnote of the table, along with its standard deviation s.

| x <sub>1</sub> | Н <sup>E</sup> <sub>m,12</sub> /<br>J mol <sup>-1</sup> а | <i>x</i> <sub>1</sub> | $H_{m,12}^{E}/J mol^{-1} a$ | <i>x</i> <sub>1</sub> | $H_{m,12}^{E}/J \text{ mol}^{-1 a}$ |
|----------------|---|-----------------------|-----------------------------|-----------------------|-------------------------------------|
| 0.0501         | 99.1  | 0.4001                | 456.6                       | 0.6500                | 410.4                               |
| 0.1000         | 184.9   | 0.4509                | 467.5                       | 0.7000                | 375.4                               |
| 0.1500         | 258.1   | 0.4999                | 463.6                       | 0.7501                | 331.8                               |
| 0.2001         | 321.3   | 0.5001                | 466.7                       | 0.8001                | 280.6                               |
| 0.2501         | 369.9   | 0.5003                | 466.0                       | 0.8501                | 221.1                               |
| 0.3000         | 409.5   | 0.5499                | 454.3                       | 0.9000                | 153.5                               |
| 0.3497         | 438.1   | 0.6003                | 436.8                       | 0.9500                | 78.8                                |

TABLE 1

Experimental results for the excess molar enthalpy  $H_{m,12}^E$  of  $x_1C_5H_{12}O + (1-x_1)C_6H_{12}$  mixtures at 298.15 K

<sup>a</sup>  $H_{m,12}^{E}/(J \text{ mol}^{-1}) = x_1(1-x_1)[1861.87 + 208.86(1-2x_1) + 36.21(1-2x_1)^2]; s = 1.0.$ 

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| cyclohexane and n-decane to form   |  |
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| molar enthalpies $H_{m,1+23}^{E}$ at 298.15 K for the addition of MTBE to a binary mixture of cy | $x + x_3 C_{10}H_3$ , and values of $H_{m_1,3}^E$ calculated from eqn. (1) using $H_{m_2,3}^E$ from ref. 3 |
| Experimental excess  | $x_1C_4H_{12}O + x_2C_6H_1$  |

| x <sup>1</sup>                       | $H_{m,1+23}^{E}/J \text{ mol}^{-1 a}$                | $H_{m,123}^{E}/J \text{ mol}^{-1}$                                   | <i>x</i> <sub>1</sub>                     | $H_{m,1+23}^{E}/J mol^{-1 a}$         | $H_{m,123}^{E}/J \text{ mol}^{-1}$ | <i>x</i> <sup>1</sup> | $H_{m,1+23}^{E}/J mol^{-1 a}$ | $H_{m,123}^{E}/J mol^{-1}$ |
|--------------------------------------|--|--|---|---------------------------------------|------------------------------------|-----------------------|-------------------------------|----------------------------|
| $x_{2}/x_{3} = 0$                    | $(3313, H_{\rm m}^{\rm E})$                          | $^{1}) = 202.5$  |   |                                       |                                    |                       |                               |                            |
| 0.0500                               | 74.9   | 267.3  | 0.4000                                    | 420.3                                 | 541.8                              | 0.7002                | 394.9                         | 455.7                      |
| 0.1000                               | 147.1  | 329.4  | 0.4496                                    | 437.4                                 | 548.9                              | 0.7501                | 357.5                         | 408.2                      |
| 0.1500                               | 211.1  | 383.3  | 0.5004                                    | 446.5                                 | 547.6                              | 0.8001                | 309.6                         | 350.1                      |
| 0.2001                               | 268.6  | 430.6  | 0.5005                                    | 446.0                                 | 547.1                              | 0.8501                | 250.1                         | 280.5                      |
| 0.2501                               | 319.6  | 471.5  | 0.5500                                    | 447.7                                 | 538.8                              | 0.9004                | 179.2                         | 199.3                      |
| 0.3000                               | 360.5  | 502.3  | 0.6002                                    | 439.2                                 | 520.2                              | 0.9500                | 96.1                          | 106.2                      |
| 0.3501                               | 394.6  | 526.2  | 0.6500                                    | 421.9                                 | 492.7                              |                       |                               |                            |
| $x_{3}/x_{3} = 1$                    | .0032, $H_{\rm m}^{\rm E}$ , $_{3}/(\rm J mol^{-}$   | $^{1}) = 319.1$  |   |                                       |                                    |                       |                               |                            |
| 0.0501                               | 72.0   | 375.1  | 0.3999                                    | 384.8                                 | 576.3                              | 0.7002                | 351.3                         | 447.0                      |
| 0.1000                               | 139.9  | 427.0  | 0.4499                                    | 399.3                                 | 574.8                              | 0.7500                | 316.8                         | 396.6                      |
| 0.1500                               | 199.8  | 471.0  | 0.5001                                    | 405.7                                 | 565.2                              | 0.8002                | 270.6                         | 334.4                      |
| 0.2000                               | 250.5  | 505.8  | 0.5503                                    | 404.6                                 | 548.0                              | 0.8500                | 218.3                         | 266.2                      |
| 0.2501                               | 296.4  | 535.7  | 0.6000                                    | 394.8                                 | 522.4                              | 0.9000                | 154.5                         | 186.4                      |
| 0.3001                               | 333.9  | 557.3  | 0.6499                                    | 377.6                                 | 489.3                              | 0.9500                | 81.6                          | 97.5                       |
| 0.3503                               | 362.8  | 570.1  |   |                                       |                                    |                       |                               |                            |
| $(x_{3})/(x_{3}) = 2$                | $(.9784, H_{\rm m}^{\rm E})^3/(.1 \text{ mol}^{-1})$ | $^{-1}$ ) = 292.2  |   |                                       |                                    |                       |                               |                            |
| 0.0500                               | 75.9   | 353.6  | 0.3998                                    | 381.2                                 | 556.6                              | 0.7000                | 333.3                         | 421.0                      |
| 0.1000                               | 143.1  | 406.1  | 0.4501                                    | 392.6                                 | 553.3                              | 0.7500                | 298.4                         | 371.5                      |
| 0.1500                               | 202.4  | 450.7  | 0.4502                                    | 392.3                                 | 553.0                              | 0.8001                | 254.2                         | 312.6                      |
| 0.2000                               | 255.2  | 489.0  | 0.5003                                    | 398.6                                 | 544.6                              | 0.8501                | 203.7                         | 247.5                      |
| 0.2500                               | 299.1  | 518.3  | 0.5501                                    | 394.8                                 | 526.3                              | 0.9000                | 143.1                         | 172.4                      |
| 0.3001                               | 334.5  | 539.0  | 0.6499                                    | 362.1                                 | 464.4                              | 0.9500                | 74.4                          | 89.0                       |
| 0.3502                               | 360.8  | 550.6  |   |                                       |                                    |                       |                               |                            |
| <sup>a</sup> Ternar.<br>5505.0 $x_1$ | / term for represen $x_2 - 4328.3x_2^2 - 4078$       | tation of $H_{m,1+2}^{E}$<br>7.7 $x_{1}^{3}$ - 28807.4 $x_{1}^{2}$ 3 | $_{2}^{3}$ by equ:<br>$_{2}$ ); $s = 3.9$ | s. (2) and (3): $H_{\rm m}^{\rm E}$ . | $x_1 x = x_1 x$                    | (-38.7)               | $(-13140.6x_1 + 735.7)$       | $x_2 + 41872.6x_1^2 +$     |

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|                | : enthalpics $H_{m,1+23}^{E}$ at 298.15 K for the addition of MTBE to a binary mixture of 23DMB and <i>n</i> -decane to form $C_{10}H_{22}$ , and values of $H_{m,123}^{E}$ calculated from eqn. (1) using $H_{m,23}^{E}$ from ref. 4 |
|----------------|---|
|                | s molar enthal $[_{14} + x_3C_{10}H_{22},$  |
| <b>FABLE 3</b> | Experimental excess $v_1 C_5 H_{12} O + x_2 C_6 H$  |

| x <sup>1</sup>                 | $H_{m,1+23}^{E}/J mol^{-1 a}$                      | $H_{m,123}^{E}/J \text{ mol}^{-1}$                                | <i>x</i> <sub>1</sub>       | $H_{m,1+23}^{E}/J mol^{-1 a}$ | $H_{m,123}^{E}/J mol^{-1}$          | x <sup>1</sup>         | $H_{m,1+23}^{E}/J \text{ mol}^{-1 a}$ | $H_{m,123}^{E}/J mol^{-1}$ |
|--------------------------------|--|---|-----------------------------|-------------------------------|-------------------------------------|------------------------|---------------------------------------|----------------------------|
| $x_2/x_3 =$                    | $0.3334, H_{m,23}^{E}/(J mol^{-})$                 | $^{1}) = 34.2$  |                             |                               |                                     |                        |                                       |                            |
| 0.0500                         | 90.9   | 123.4   | 0.3999                      | 449.7                         | 470.3                               | 0.6999                 | 416.2                                 | 426.4                      |
| 0.1000                         | 169.1  | 199.9   | 0.4502                      | 467.8                         | 486.6                               | 0.7501                 | 377.3                                 | 385.9                      |
| 0.1500                         | 236.1  | 265.2   | 0.5002                      | 479.0                         | 496.1                               | 0.8049                 | 320.1                                 | 326.8                      |
| 0.1999                         | 296.6  | 324.0   | 0.5003                      | 474.5                         | 491.7                               | 0.8500                 | 265.4                                 | 270.5                      |
| 0.2511                         | 345.8  | 371.5   | 0.5500                      | 476.3                         | 491.7                               | 0.9000                 | 191.7                                 | 195.1                      |
| 0.3000                         | 390.1  | 414.0   | 0.6000                      | 467.5                         | 481.2                               | 0.9500                 | 105.3                                 | 107.0                      |
| 0.3502                         | 425.6  | 447.8   | 0.6499                      | 444.1                         | 456.1                               |                        |                                       |                            |
| $(x_{2}/x_{3}) =$              | $1.0000, H_{\rm m}^{\rm E}$ 33/(J mol <sup>-</sup> | $^{1}) = 46.8$  |                             |                               |                                     |                        |                                       |                            |
| 0.0499                         | 91.6   | 136.0   | 0.4000                      | 401.3                         | 429.4                               | 0.7002                 | 365.1                                 | 379.2                      |
| 0.1001                         | 156.9  | 199.0   | 0.4501                      | 415.3                         | 441.1                               | 0.7479                 | 333.3                                 | 345.1                      |
| 0.1500                         | 216.8  | 256.5   | 0.4998                      | 422.4                         | 445.8                               | 0.8000                 | 284.3                                 | 293.7                      |
| 0.2001                         | 267.7  | 305.1   | 0.4999                      | 421.6                         | 445.0                               | 0.8502                 | 230.1                                 | 237.1                      |
| 0.2499                         | 307.7  | 342.8   | 0.5497                      | 419.3                         | 440.4                               | 0.9000                 | 166.5                                 | 171.1                      |
| 0.3000                         | 349.2  | 382.0   | 0.5998                      | 409.7                         | 428.4                               | 0.9500                 | 91.6                                  | 94.0                       |
| 0.3498                         | 379.2  | 409.6   | 0.6499                      | 392.0                         | 408.3                               |                        |                                       |                            |
| $x_2/x_3 =$                    | $3.0080, H_{m,23}^{E}/(J \text{ mol}^{-})$         | $^{1}) = 35.9$  |                             |                               |                                     |                        |                                       |                            |
| 0.0500                         | 68.3   | 102.4   | 0.4001                      | 342.1                         | 363.7                               | 0.7001                 | 301.1                                 | 311.9                      |
| 0.1000                         | 131.1  | 163.4   | 0.4501                      | 348.9                         | 368.7                               | 0.7500                 | 272.7                                 | 281.7                      |
| 0.1500                         | 183.1  | 213.6   | 0.5000                      | 355.7                         | 373.6                               | 0.8000                 | 230.6                                 | 237.7                      |
| 0.2000                         | 230.6  | 259.3   | 0.5000                      | 355.4                         | 373.4                               | 0.8500                 | 186.3                                 | 191.7                      |
| 0.2501                         | 262.8  | 289.7   | 0.5498                      | 353.7                         | 369.9                               | 0.9000                 | 129.9                                 | 133.5                      |
| 0.3001                         | 298.2  | 323.3   | 0.6003                      | 343.6                         | 358.0                               | 0.9500                 | 70.0                                  | 71.8                       |
| 0.3502                         | 323.8  | 347.1   | 0.6498                      | 329.3                         | 341.9                               |                        |                                       |                            |
| <sup>a</sup> Ternai<br>10005.3 | y term for represent $x_1x_2 - 1223.9x_2^2 - 1842$ | (ation of $H_{\rm m,1+23}^{\rm E}$<br>38.9 $x_1^3 - 25778.8x_1^2$ | by eqns. $x_2$ ); $s = 2$ . | (2) and (3): $H_{m,I}^{E}$    | $x_1(J \text{ mol}^{-1}) = x_1 x_2$ | x <sub>3</sub> (3023.2 | $-13002.2x_1 - 2318.0x_2$             | $x_2^2 + 29364.6x_1^2 + $  |



Fig. 1. Excess molar enthalpies  $H_{m,1+23}^{E}$  at 298.15 K for the addition of MTBE to binary mixtures of cyclohexane and *n*-decane to form  $x_1C_5H_{12}O + x_2C_6H_{12} + x_3C_{10}H_{22}$ . Experimental results:  $\Box$ ,  $x_2/x_3 = 0.3313$ ;  $\bigcirc$ ,  $x_2/x_3 = 1.0032$ ;  $\diamondsuit$ ,  $x_2/x_3 = 2.9784$ ;  $\bigtriangledown$ ,  $x_3 = 0$ . Curves: ---,  $x_3 = 0$ , calculated from the representation in the footnote of Table 1; ...,  $x_2 = 0$ , calculated from the representation in ref. 1; ----, calculated from eqn. (2) with  $H_{m,T}^{E}$  from the footnote of Table 2; ---, calculated from the Flory theory.

The experimental results for  $H_{m,1+23}^{E}$  and the corresponding values of  $H_{m,123}^{E}$  are listed in Tables 2 and 3 for the two ternary systems. The values of  $H_{m,1+23}^{E}$  are plotted in Figs. 1 and 2. The results for  $H_{m,12}^{E}$  from Table 1 can be identified with  $H_{m,1+23}^{E}$  for the case  $x_3 = 0$ , and are included in Fig. 1 for comparison.

 $H_{m,1+23}^{E}$  was represented as a sum of binary terms [5] with an added ternary contribution

$$H_{m,1+23}^{E} = \left(\frac{x_{2}}{1-x_{1}}\right) H_{m,12}^{E} + \left(\frac{x_{3}}{1-x_{1}}\right) H_{m,13}^{E} + H_{m,T}^{E}$$
(2)

where values of  $H_{m,ij}^{E}$  were calculated from the appropriate smoothing functions as given either in Table 1 or in the literature [1, 6]. Following Morris et al. [7], the form



Fig. 2. Excess molar enthalpies  $H_{m,1+23}^{E}$  at 298.15 K for the addition of MTBE to binary mixtures of 23DMB and *n*-decane to form  $x_1C_5H_{12}O + x_2C_6H_{14} + x_3C_{10}H_{22}$ . Experimental results:  $\Box$ ,  $x_2/x_3 = 0.3334$ ;  $\bigcirc$ ,  $x_2/x_3 = 1.0000$ ;  $\diamondsuit$ ,  $x_2/x_3 = 3.0080$ . Curves: ---,  $x_3 = 0$ , calculated from the representation in ref. 6;  $\cdots$ ,  $x_2 = 0$ , calculated from the representation in ref. 1; ---, calculated from eqn. (2) with  $H_{m,T}^{E}$  from the footnote of Table 3; ---, calculated from the Flory theory.

$$H_{m,T}^{E} = x_1 x_2 x_3 (c_0 + c_1 x_1 + c_2 x_2 + c_3 x_1^2 + c_4 x_1 x_2 + c_5 x_2^2 + \dots)$$
(3)

was adopted for the ternary term. Values of the parameters  $c_i$  were obtained from least-squares analyses in which eqns. (2) and (3) were fitted to the experimental results for the ternary systems. These representations are given in the footnotes of Tables 2 and 3, along with their standard deviations s; curves calculated from them are shown in Figs. 1 and 2.

Some enthalpy contours corresponding to constant values of  $H_{m,123}^{E}$  are plotted on the Roozeboom diagrams shown in Figs. 3 and 4. Previously, for the MTBE + *n*-hexane + *n*-decane system [1], the maximum of  $H_{m,123}^{E}$  was located on the edge of the triangle in the constituent MTBE + *n*-decane binary. In Fig. 3, where *n*-hexane has been replaced by its branched isomer 23DMB, the maximum of  $H_{m,123}^{E}$  has increased only slightly and although it



Fig. 3. Contours for constant values of the excess molar enthalpy  $H_{m,123}^{E}/(J \text{ mol}^{-1})$  of the MTBE + 23DMB + *n*-C<sub>10</sub>H<sub>22</sub> system at 298.15 K, calculated from eqns. (1) and (2) using  $H_{m,T}^{E}$  from the footnote of Table 3.

is located inside the triangle, it is still fairly close to the edge. However, for the system with cyclohexane (Fig. 4), the maximum of  $H_{m,123}^E$  has increased by about 70 J mol<sup>-1</sup>, and is more centrally located in the triangle.

Previously, for MTBE + *n*-hexane + *n*-decane [1], it was found that the Flory theory [8, 9], as extended by Brostow and Sochanski [10], provided reasonable estimates of the ternary enthalpies when only data for the pure components and their binary mixtures were used. The same approach was investigated for the present systems. Because the treatment follows our previous work closely, only the primary data and the results of the calculations are reported here. The component properties [1, 11–13] and parameters are summarized in Table 4, where the notation is the same as defined in ref. 1. The results of the calculations of  $H_{m,1+23}^E$  are shown as broken curves in Figs. 1 and 2. For the 58 points of the cyclohexane system (given in Table 2), the standard deviation between the estimated and experimental values of  $H_{m,123}^E$  is 8.8 J mol<sup>-1</sup>, and the mean absolute relative deviation is 2.2%. For the 60 points of the 23DMB system (given in Table 3), the corresponding deviations are 18.5 J mol<sup>-1</sup> and 5.1%. Although these deviations are larger



Fig. 4. Contours for constant values of the excess molar enthalpy  $H_{m,123}^{E}/(J \text{ mol}^{-1})$  of the MTBE + c-C<sub>6</sub>H<sub>12</sub> + n-C<sub>10</sub>H<sub>22</sub> system at 298.15 K, calculated from eqns. (1) and (2) using  $H_{m,T}^{E}$  from the footnote of Table 2.

#### TABLE 4

| Component                                 | $V_{\rm m}/{ m cm^3~mol^{-1}}$ | $rac{lpha_p}{kK^{-1}}$ | κ <sub>T</sub> /<br>TPa <sup>-1</sup> | <i>P*/</i><br>J cm <sup>-3</sup> | $V^*/$ cm <sup>3</sup> mol <sup>-1</sup> | Т*/<br>К | Ref. |
|---|--------------------------------|-------------------------|---------------------------------------|----------------------------------|--|----------|------|
| $\frac{1}{C_5H_{12}O}$ (MTBE)             | 119.82                         | 1.423                   | 1690.6                                | 442.9                            | 90.20                                    | 4385.0   | 1    |
| C <sub>6</sub> H <sub>12</sub>            | 108.75                         | 1.220                   | 1140.0                                | 532.0                            | 84.23                                    | 4715.0   | 11   |
| C <sub>6</sub> H <sub>14</sub><br>(23DMB) | 131.16                         | 1.391                   | 1790.2                                | 405.3                            | 99.16                                    | 4430.2   | 12   |
| $C_{10}H_{22}$                            | 195.94                         | 1.051                   | 1109.6                                | 447.0                            | 155.75                                   | 5091.4   | 13   |

Component properties and parameters used in Flory calculations for the systems  $x_1C_5H_{12}O + x_2C_6H_{12} + x_3C_{10}H_{22}^{\ a}$  and  $x_1C_5H_{12}O + x_2C_6H_{14} + x_3C_{10}H_{22}^{\ b}$  at 298.15 K

Interchange interaction parameters  $X_{ij}/(J \text{ cm}^{-3})$ : <sup>a</sup>  $X_{12} = 20.1640$ ;  $X_{13} = 18.7764$ ;  $X_{23} = 12.4736$ . <sup>b</sup>  $X_{12} = 12.3507$ ;  $X_{13} = 18.7764$ ;  $X_{23} = 2.3015$ .

than those found previously for MTBE + n-hexane + n-decane, it appears that the Flory treatment can provide estimates of the enthalpies of the present systems within less than 10%.

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